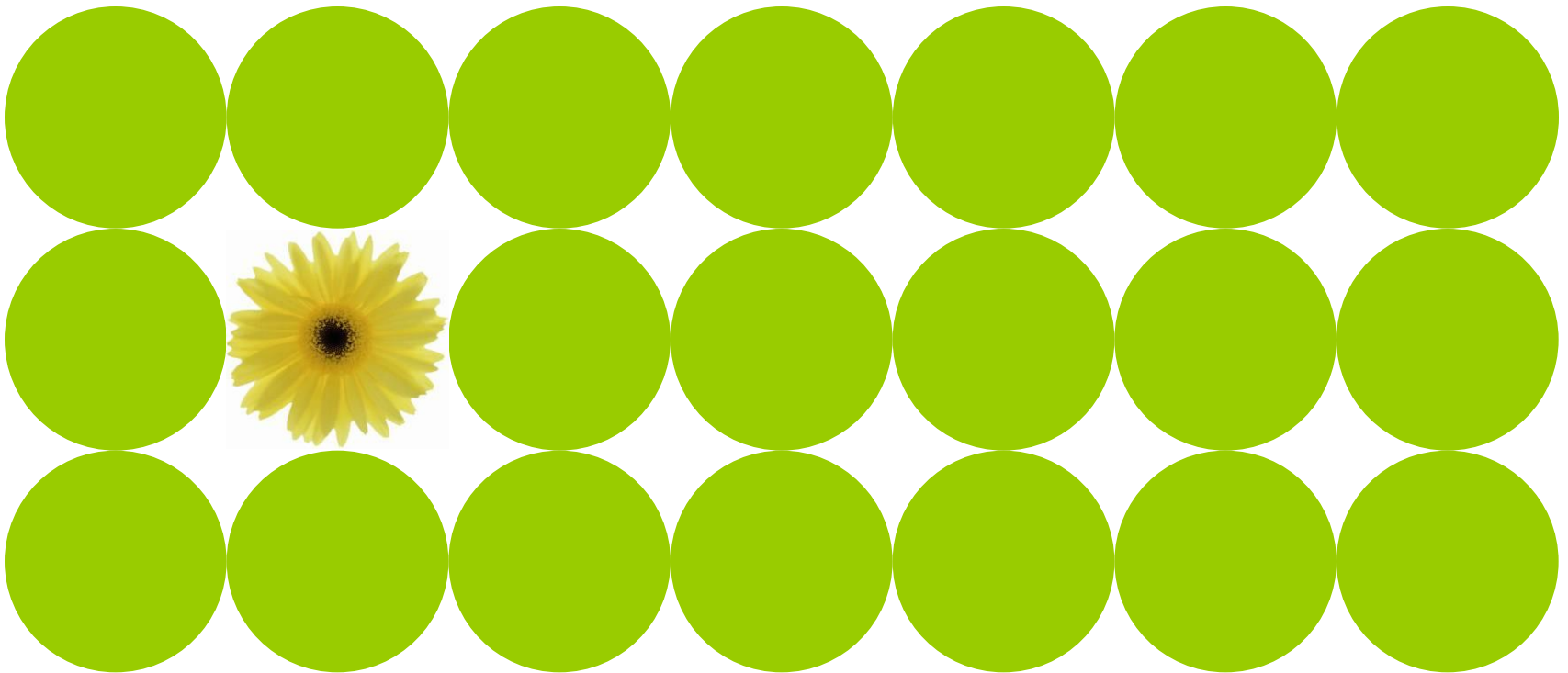


Emissions from Su3 and Su4 at Hydro Sunndal



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February 2009

Potlines at Hydro Sunndalsøra Norway

Søderberg line

- Started in 1954-1959, 264+36 cells operating at 86 kA
- Shut down in 2002

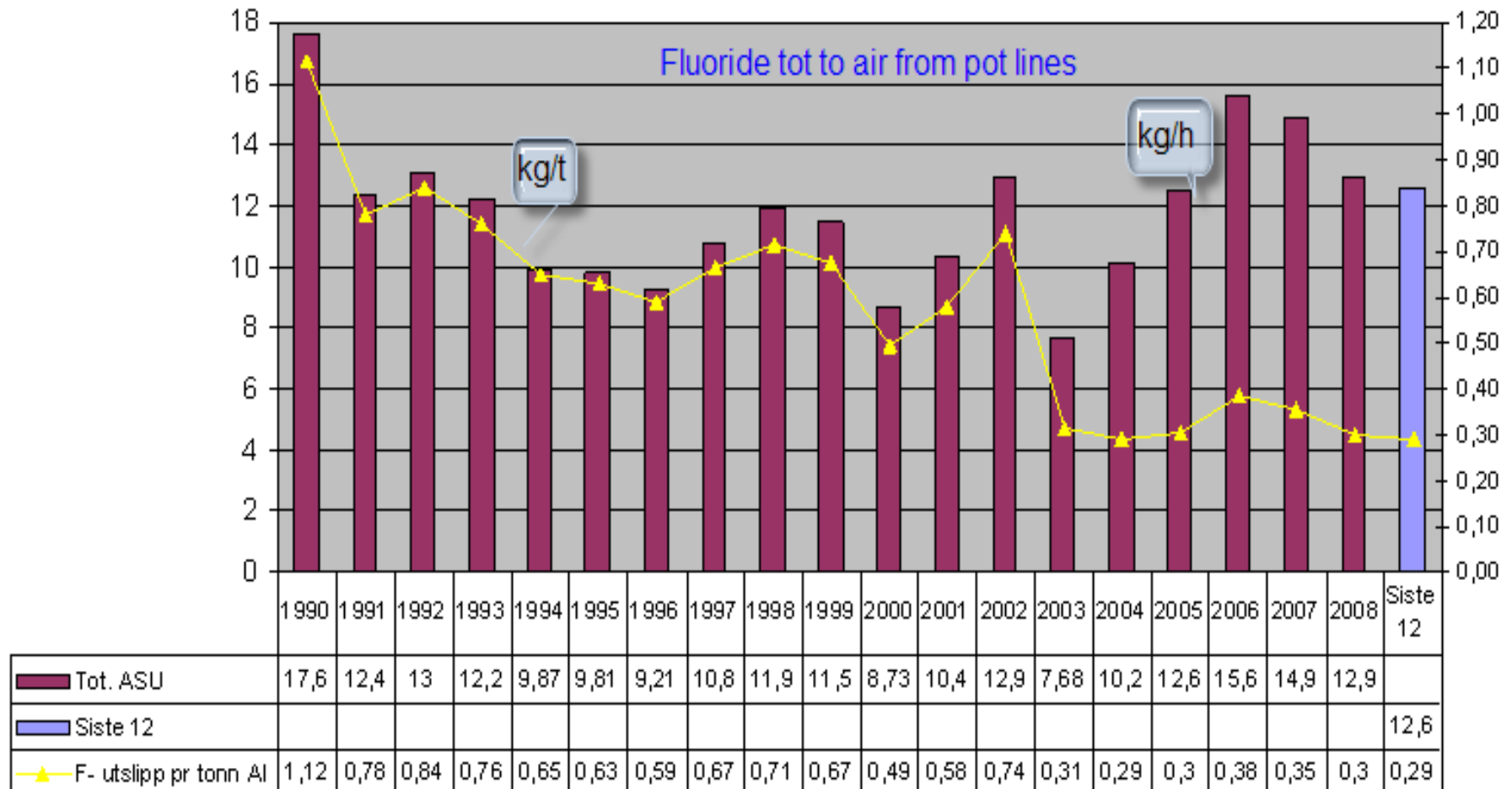
Su3

- Started in 1969, Alcan Technology, end-to-end cells
- Started at 135 kA and currently operating with point feeders at 202 kA

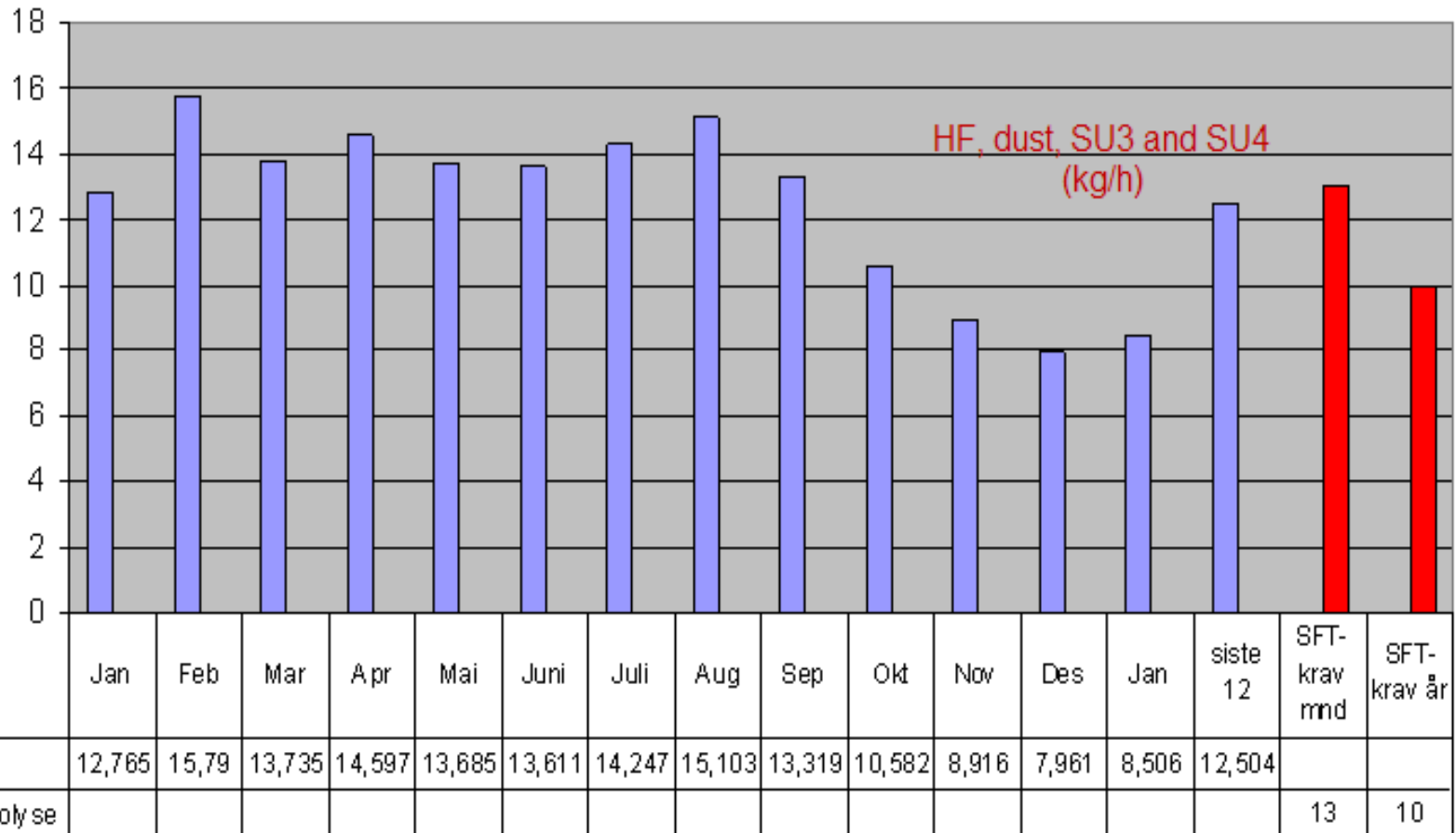
Su4

- Built in 2002, Hydro technology, side-by-side cells
- Started at 252 kA and currently operating at 302 kA
 - An upgraded version of this cell will be installed in Qatar

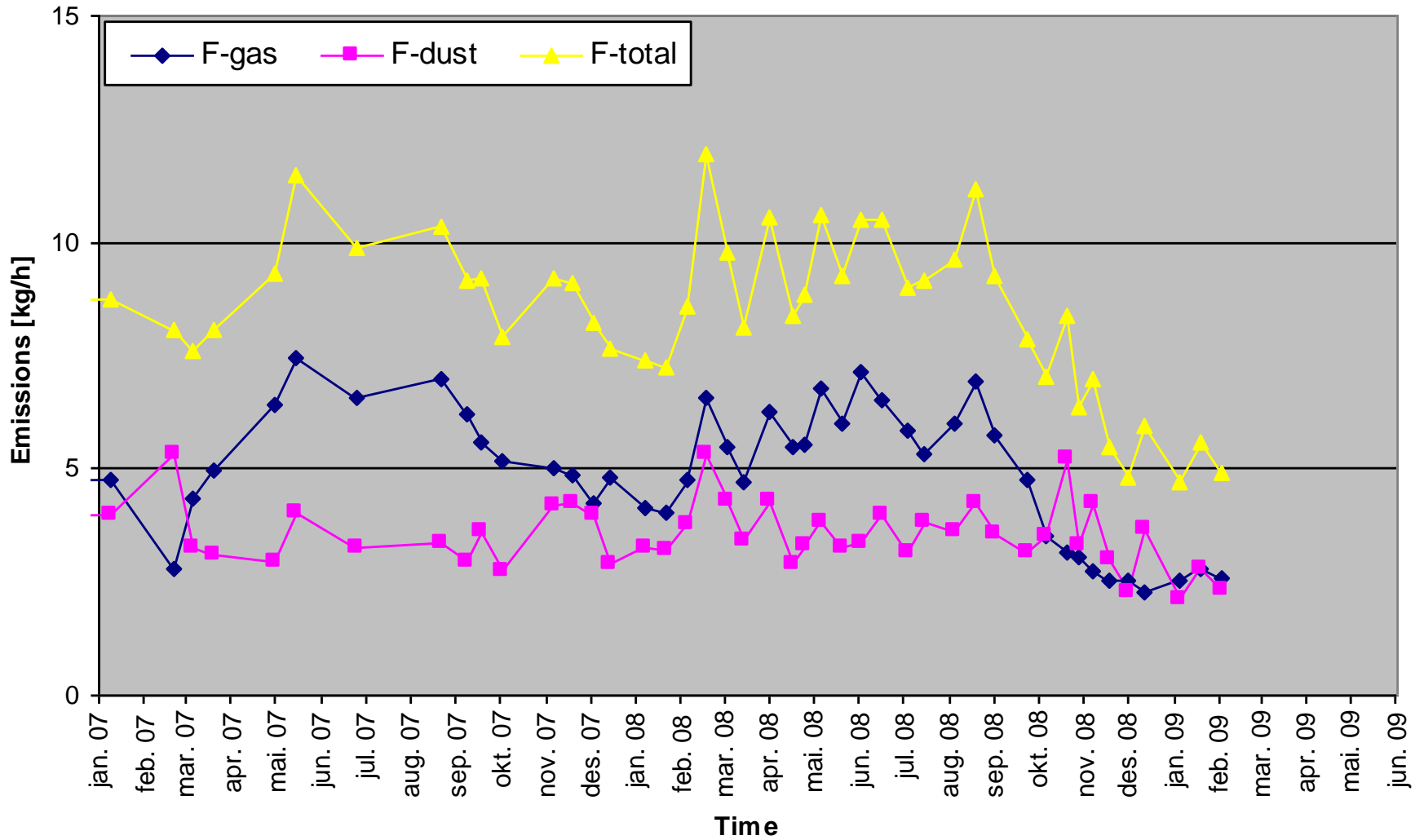
Total Fluoride Emission to Air 1990 - 2008



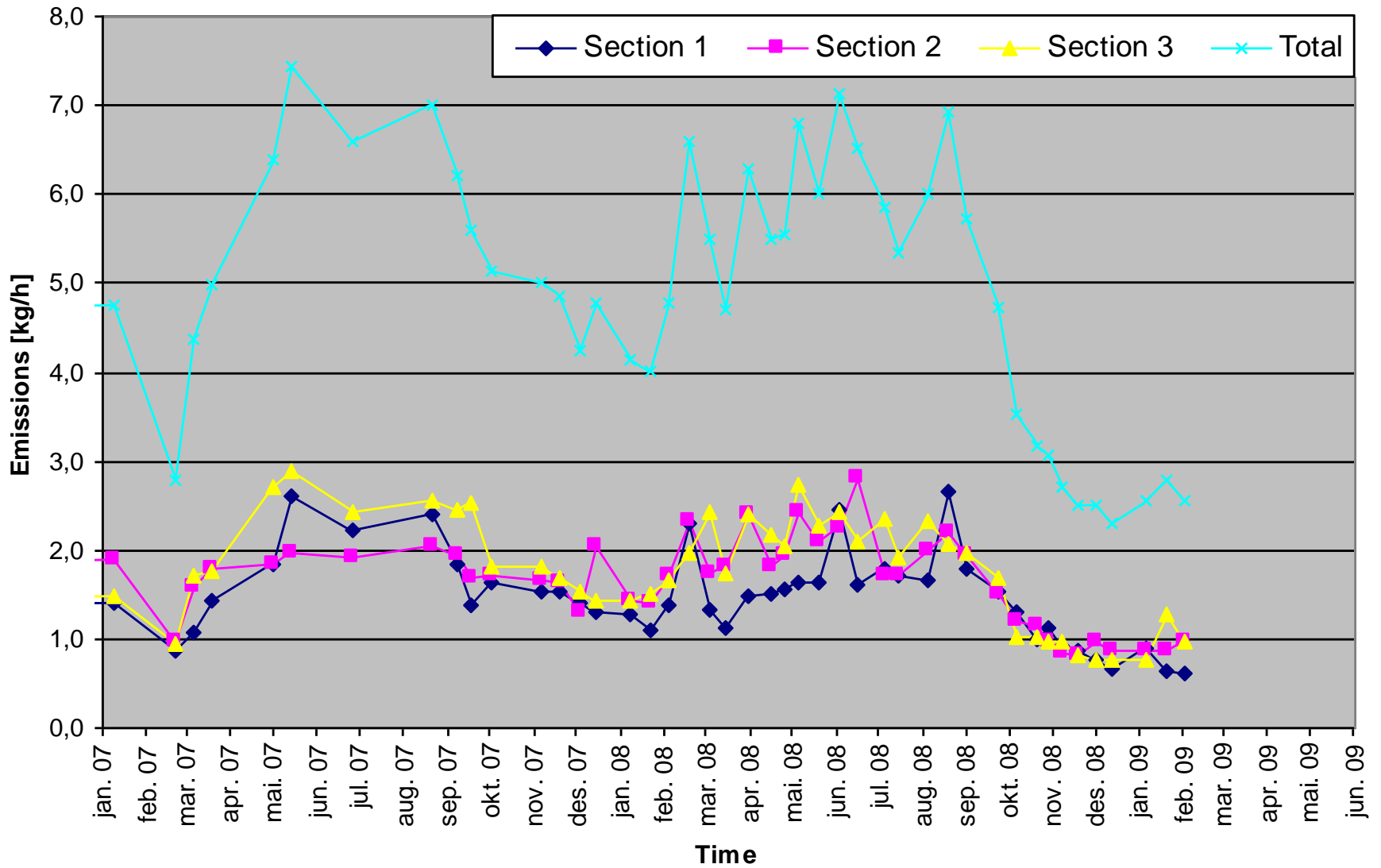
Total Fluoride Emission SU3 and SU4 2008 – 2009 (kg/h)



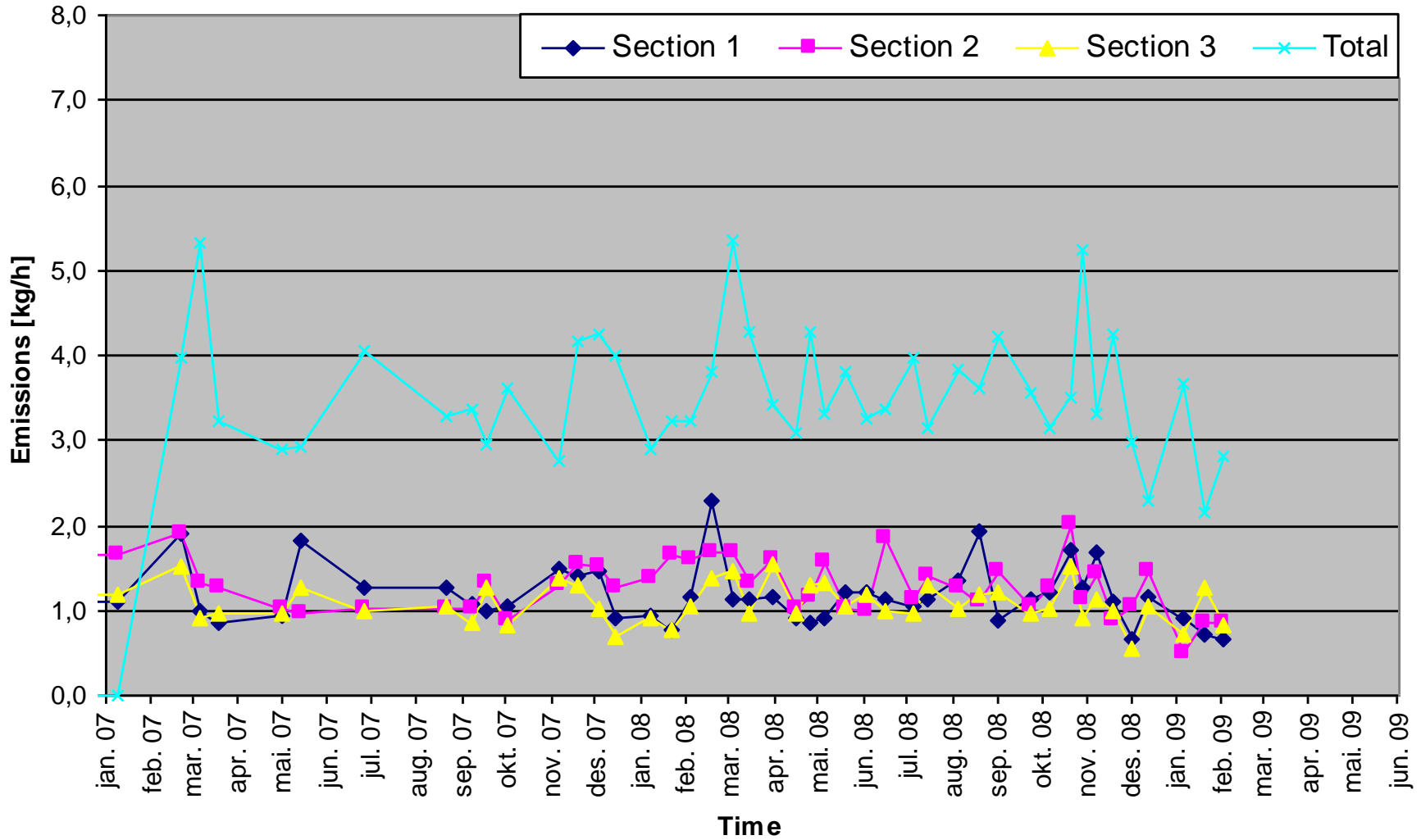
Fluoride-emissions in Su4



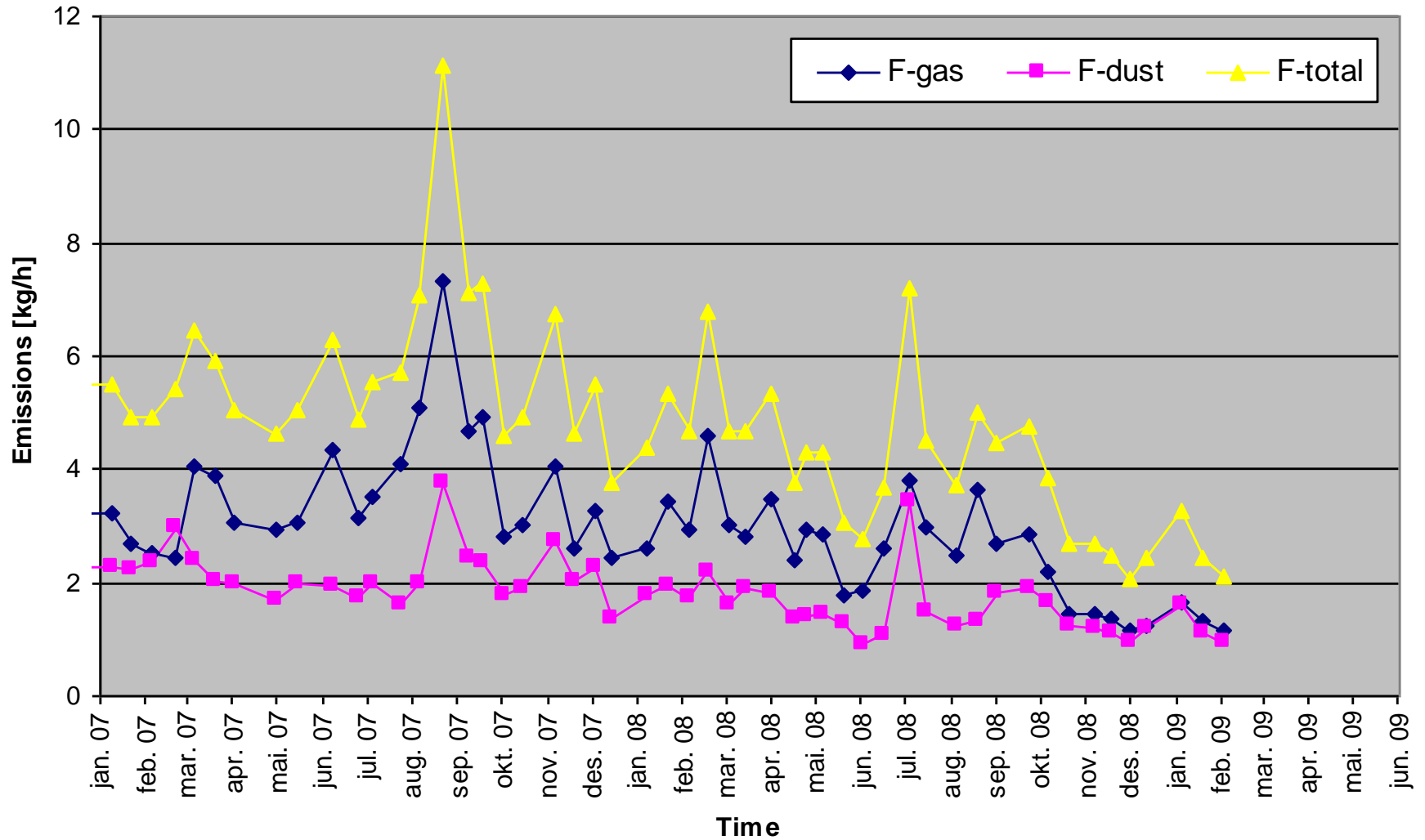
HF-emissions from Su4



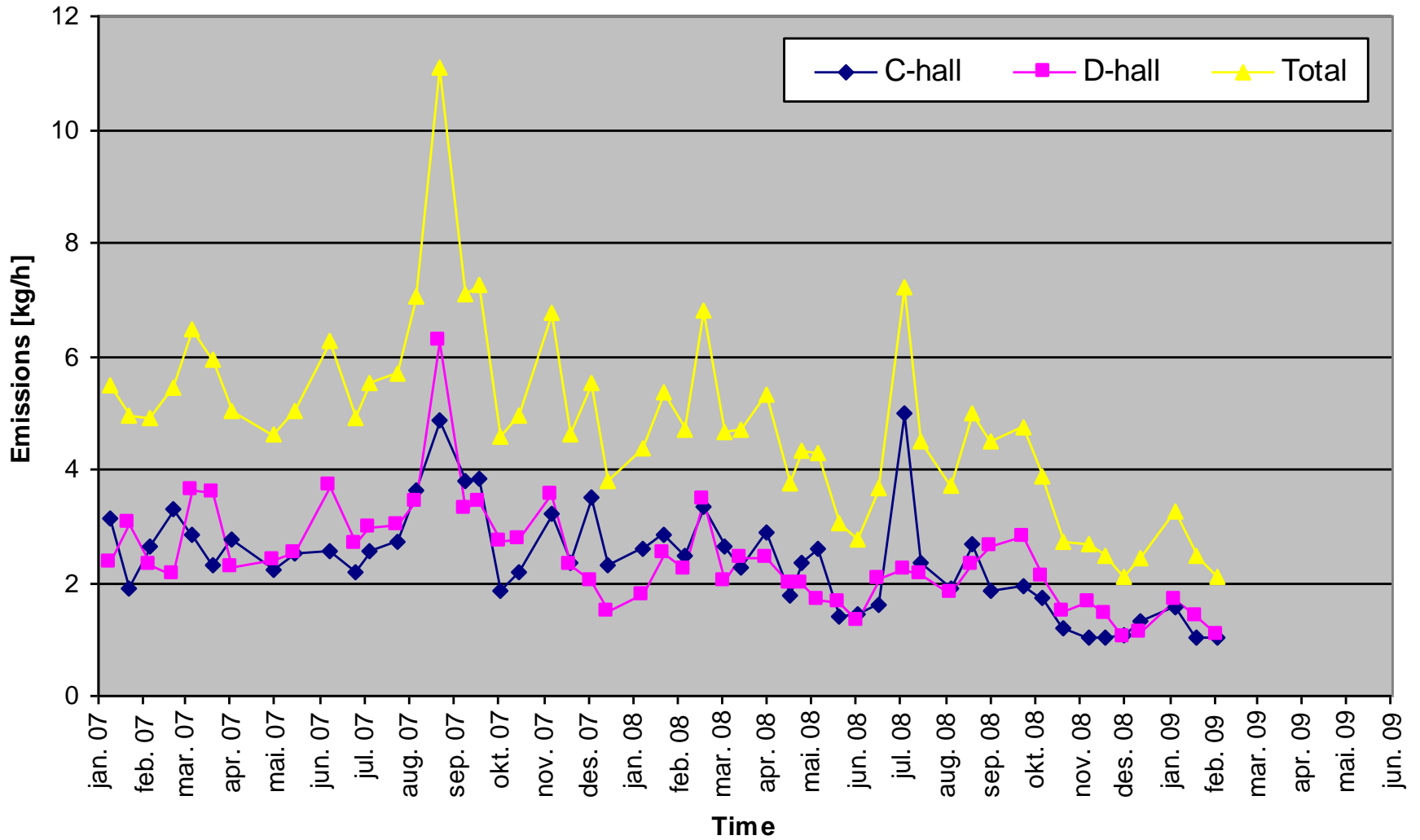
Fluoride-emissions (dust form) from Su4



Fluoride-emissions from Su3



Fluoride emissions from Su3 - (gas and dust in total)



Main Actions to Lower Fluoride Emissions Autumn-Winter 2008 (1)

Upgrading of scrubbers to increase suction capacity.

- From 5500 to 6500 Nm³/h per cell in Su4
- From 5000 Nm³ to 7000 Nm³/h per cell in SUIII
- Forced suction in Su4 increased from 15000 to 18000 Nm³/h
 - Maximum two cells per 15 cell at forced suction at the same time
 - Suction rate on environmental boxes is increased

Systematic mapping of status on suction canals, from the scrubbers to each cell, by measuring under pressure and air flow.

- Focus on high hooding efficiency on the cells.

Main Actions to Lower Fluoride Emissions Autumn-Winter 2008 (2)

Balancing suction rate, to secure right amount of suction from each cell.

Cleaning and improving old suction channels in SU3.

Focus on operational routines giving fluoride emissions.

New preheat and start up procedures in Su4

- Coke preheat with no skimming of carbon dust

How to reduce Green House Gas Emissions?

How to Reduce Greenhouse Gas Emissions

1. CO₂ - **Reduce net anode consumption**
2. PFC - **Reduce the number of anode effect minutes per cell-day by:**
 - **Reduce anode effect frequency**
 - **Reduce anode effect duration**

Green House Gas Emissions

Greenhouse gas emissions from aluminium electrolysis cells:

CO₂ from electrolysis:



(Global Warming Potential, GWP = 1)

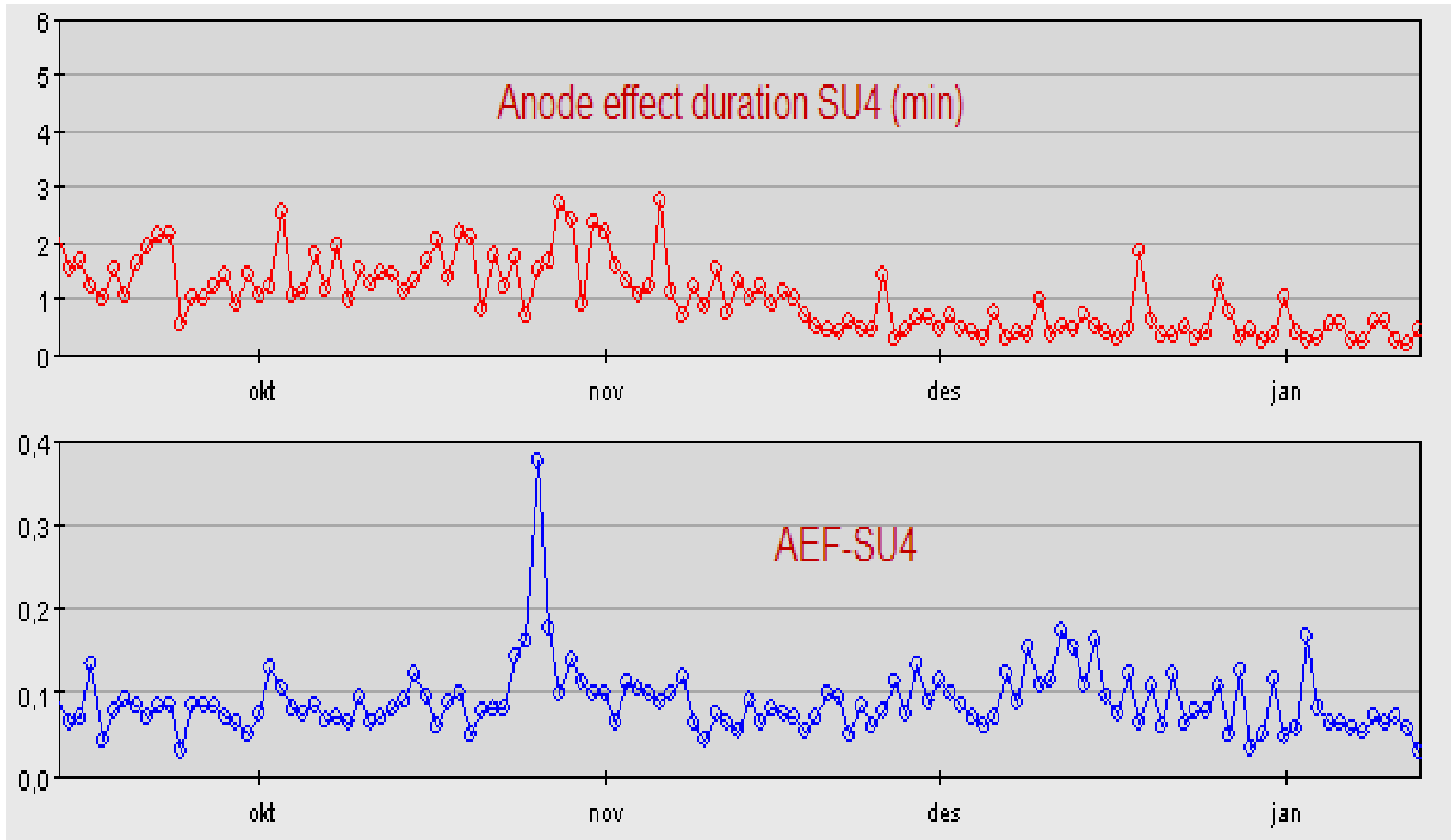
PFCs:

CF₄ from anode effects (GWP = 6500)

C₂F₆ from anode effects (GWP = 9200)

(C₂F₆ is typically 5 to 12 % of the amount of CF₄)

CF4 and C2F6 Emissions From Su4 (daily average figures)



Automatic Anode effect Quenching

An effective strategy has the following objectives:

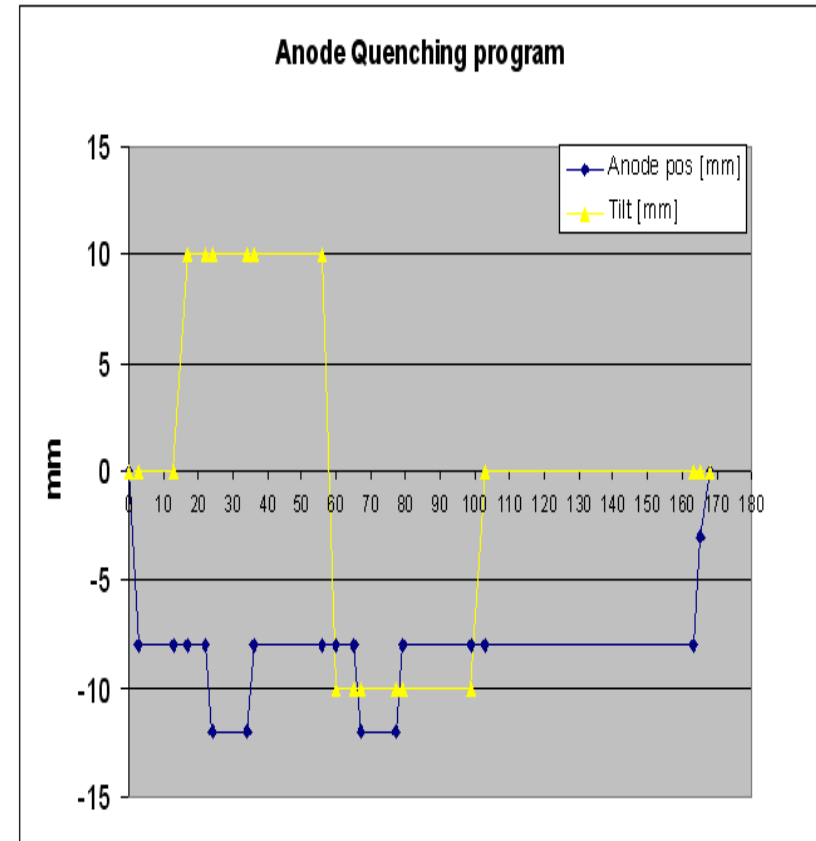
- Minimize the energy input to the cell.
- Avoid extensive anode movement.
- Optimize alumina addition.

The results from a successful strategy are:

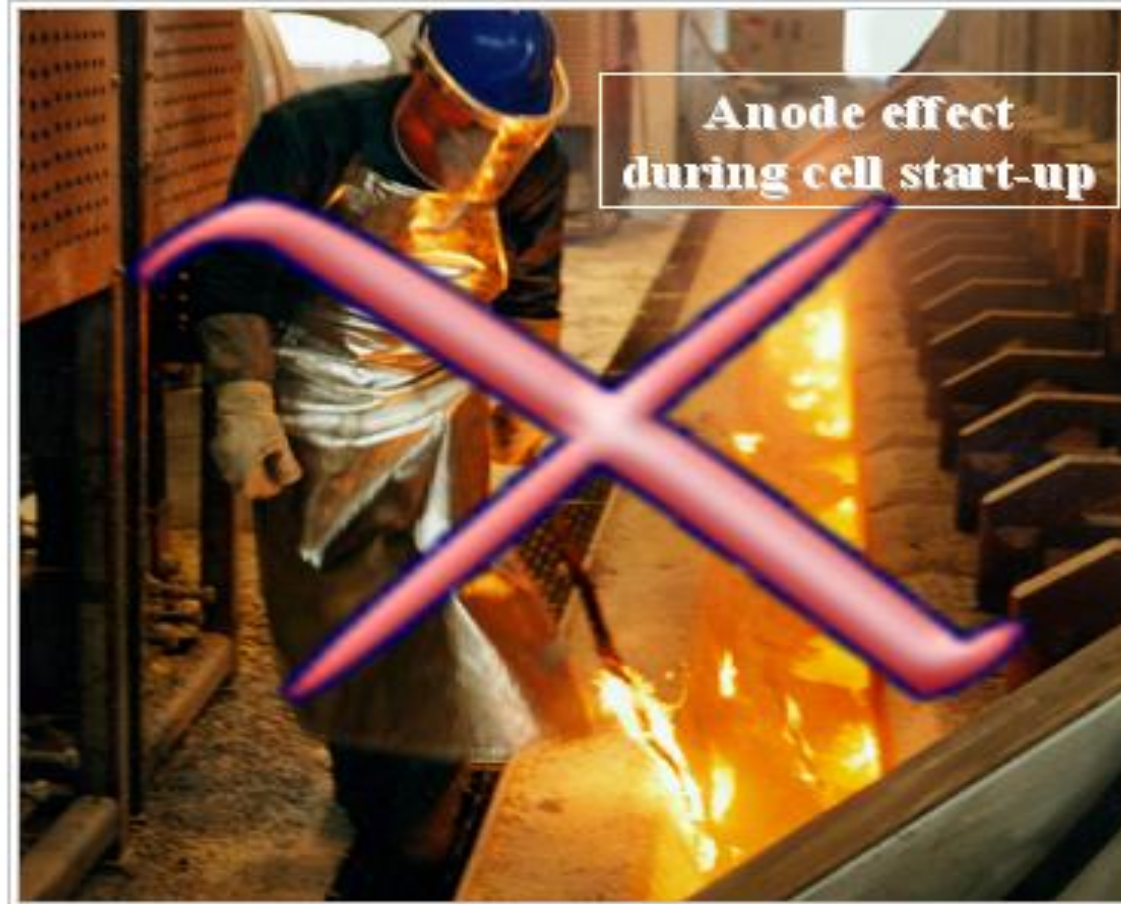
High percentage of successful quenching. (70-90%)

Short recovery time after anode effect. (0-1h)

Low anode effect duration. (<45 s)



Anode Effect During Start Up



Anode Effect During Start Up



Net Anode Consumption

Net Anode Consumption

- What is the theoretical (electrolytic) anode consumption?
The reaction: $2 \text{Al}_2\text{O}_3 + 3\text{C} = 4 \text{Al} + 3 \text{CO}_2$ gives **333 kg C/t Al**

- What is the extra contribution from current efficiency (CE)?
The back reaction is: $2 \text{Al} + 3 \text{CO}_2 = \text{Al}_2\text{O}_3 + 3\text{CO}$
The net anode consumption then is: $333/(100/\%CE)$ (kg/t Al)
Thus, 95% CE gives 351 kg C/t Al, while 90% CE gives 370 kg C/t Al

- What is the excess (non-electrolytic) anode consumption?
 1. Reaction of carbon with O_2 at the exposed anode top surface (airburn)
This gives a loss of 30 – 70 kg C/t Al
 2. Reaction of carbon with CO_2 in the exposed burn area at the bottom (carboxy attack: $\text{CO}_2 + \text{C} = 2 \text{CO}$)
This gives a loss of 20 – 30 kg C/t Al

Calculating CO2 emission from Net Anode Consumption

Calculation of Carbon Dioxide Emissions from Prebake Anode Consumption During Electrolysis

$$E_{CO_2} = \left[MP \times NAC \times \left(\frac{100 - S_a - Ash_a}{100} \right) \right] \times \frac{44}{12}$$

E_{CO_2} = CO₂ emissions in tonnes per year

MP = Total metal production, tonnes aluminium per year

NAC = Net anode consumption, tonnes per tonne aluminium

S_a = Sulphur content in baked anodes, wt%

Ash_a = Ash content in baked anodes, wt%

$44/12$ = CO₂ Molecular Mass : Carbon Atomic Mass Ratio, dimensionless

Physical Specification on Anode Quality

Physical properties:

| Function | Unit | Lot average | Accepted deviation in lot | Method |
|-----------------------------------|------|-------------|---------------------------|-------------|
| Equivalent temperature | | ≥ 1230 | | ISO 17499 |
| Dust by CO ₂ oxidation | | ≤ 3.0 | | TOS Årdal |
| Baked bulk density | | ≥ 1.59 | | ISO 12985-1 |
| Specific electric resistance | | ≤ 53.0 | | ISO 11713 |
| Air oxidation reactivity | | ≤ 30.0 | | TOS Årdal |
| Permeability | | ≤ 0.5 | | ----- |
| Thermal conductivity | | <3.0, 4.2> | | ISO 12987 |
| Thermal expansion coefficient | | ≤ 4.2 | | ISO 14420 |
| Flexural strength | | ≥ 12.0 | | ISO 12986-1 |
| Compressive strength | | ≥ 35 | | ISO 18515 |

(Functions/properties are "ranked", i.e. those at the top are considered more important with respect to operational performance in the electrolysis than those close to the bottom.)

Conclusion

Over the last year for the Hydro Sunndalsøra plant:

The total fluoride emission from the two lines has been reduced significantly by increasing the dry scrubber capacity and improving the operational routines

- Targeting 0.2 kg Ftot per tonne aluminium in 2009

The PFC emissions has been reduced by approximately 70 - 80 % by implementing an effective automatic anode effect quenching program and start-ups without anode effects

The net anode consumption has been improved by implementing anode quality with reduced carboxy and air reactivity



HYDRO

Thank you for your attention